UNITED STATES PATENT APPLICATION

METHOD AND POLAR-LOOP TRANSMITTER WITH ORIGIN OFFSET FOR ZERO-CROSSING SIGNALS

INVENTOR

Eliav Zipper

METHOD AND POLAR-LOOP TRANSMITTER WITH ORIGIN OFFSET
FOR ZERO-CROSSING SIGNALS

Field of the Invention

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The present invention pertains to transmitters, and in particular, pertains to modulating and amplifying an information signal for further transmission through a radio channel.

10 ### Background of the Invention

In a communication system, before a signal is modulated onto a carrier wave having an intermediate frequency, it is referred to as a baseband signal. In a transmitter, the baseband signal may be split into I and Q components that make up a vector defining the information signal. The I and Q components are
15 modulated onto a carrier wave using a modulator and the output is up-converted using one or more frequency mixers. The carrier wave includes the amplitude and phase components of the modulating signal. Because the modulator operates at relatively low power levels compared to the transmitted power level,
20 amplification between the modulator and the antenna is necessary. This amplification should be linear and efficient. Non-linear amplification creates distortion that may cause, among other things, error in the information vector. In a worst case, distortion may cause broadening of the frequency spectrum of the transmitted signal. Broadening of the frequency spectrum may interfere with
25 nearby channels and may reduce traffic capacity. It may also result in the consumption of additional power reducing the efficiency of the transmitter which is undesirable, especially for mobile communication devices.

Linear amplifiers have been used to help improve the linearity of the output signals, but their efficiency is too low to be a practical alternative to non-
30 linear power amplifiers, especially for mobile communication devices. Pre-distortion of the I and Q components is another technique that has been used to improve linearity but it is difficult to implement and it's application is limited. Cartesian feedback is another technique used for improving linearity, however this technique requires exact phase matching at the power amplifier output.

Polar-loop transmitters have also been used to help reduce spectrum broadening and improve power amplifier linearity. In a conventional polar-loop transmitter, an information signal is split into its polar components which consist of a phase reference component and an amplitude reference component. The

5   components are processed in separate control loops and recombined to produce an output signal. One problem with conventional polar-loop transmitters is that modern communication techniques introduce modulation schemes, including for example, Code Division Multiple Access (CDMA) and Wideband (CDMA) schemes, where the instant signal trajectory may cross the zero point on a phasor

10   diagram. This zero-crossing trajectory creates several difficulties for conventional polar-loop transmitters. For example, a zero-crossing trajectory has a phase component discontinuity similar to a step-function that results from the instantaneous transition of the phase by 180 degrees. The amplitude component at this zero-crossing occurrence may also contain a time derivative discontinuity.

15   Because of the zero crossing, both the amplitude and phase components become very wideband making the processing of these components sensitive to bandwidth and slew-rate limitations.

Another problem with conventional polar-loop transmitters is the processing of the phase component by a phase detector. A phase detector's

20   transfer function typically depends on the amplitude of the incoming signal, and amplitude regulating circuitry removes the amplitude modulation component. The amplitude regulating circuitry, such as a limiter or an automatic level control (ALC) circuit, has a limited range of functionality and has difficult handling zero-crossing trajectories.

25   Thus there is a general need for an improved transmitter and method for transmission of signals. There is also a need for a transmitter and method for transmission of signals with improved efficiency. There is also a need for a transmitter and method for transmission of signals that helps reduce the broadening of the frequency spectrum. There is also a need for a transmitter and

30   method for transmission of signals that helps increase the efficiency of a transmitter's non-linear amplifier. There is also a need for a transmitter and method for transmission of signals with improved linearity. There is also a need for an improved polar-loop transmitter and method that handles zero-crossing trajectories.

Brief Description of the Drawings

The invention is pointed out with particularity in the appended claims.
However, a more complete understanding of the present invention may be derived
by referring to the detailed description when considered in connection with the
figures, wherein like reference numbers refer to similar items throughout the
figures and:

FIG. 1 is a functional block diagram of a transmitter in accordance with an
embodiment of the present invention; and

FIG. 2 is a flow chart of an output signal transmission procedure in
accordance with an embodiment of the present invention.

Detailed Description

The description set out herein illustrates the various embodiments of the
invention and such description is not intended to be construed as limiting in any
manner. The present invention relates to transmitters, and in one embodiment,
relates to polar-loop transmitters. In other embodiments, the present invention
relates to transmitters for code division multiple-access (CDMA) signals
including wideband CDMA (WCDMA) signals.

FIG. 1 is a functional block diagram of a transmitter in accordance with an
embodiment of the present invention. Transmitter 100 receives a complex input
signal from a signal source. The complex input signal may be a baseband
information signal and may be at, for example, an intermediate frequency (IF).
The baseband signal, for example, may be comprised of I and Q components or
may be comprised of amplitude and phase components. The complex input signal
is combined with a compensated origin offset complex signal in input combining
element 104 to generate an offset input signal. Input phase detector 106 extracts
the phase information from the offset input signal and input amplitude detector
108 extracts the amplitude information from the offset input signal. Phase
difference element 110 generates a phase reference signal from phase information
extracted by phase detector 106 and an offset output signal. Amplitude difference
element 112 generates an amplitude reference signal from amplitude information

extracted by amplitude detector 108 and the offset output signal. Signal synthesizer 118 generates an output signal from the amplitude reference signal and the phase reference signal provided by elements 112 and 110 respectively. Elements 112 and 110 may include gain and/or filtering functionality and, for

5 example, may include a filter and/or amplifier to process either the amplitude difference or phase difference.

The output signal from signal synthesizer 118 may be amplified by non-linear amplifier 120 to produce an output signal of the transmitter. The amplified output signal is sampled by coupling element 128. Coupling element 128 may be

10 a signal coupler or other element that couples the output signal. Output combining element 122 combines the sampled/coupled output signal with an origin-offset signal to generate the offset output signal. Feedback phase detector 114 extracts phase information from the offset output signal, and feedback amplitude detector 116 extracts amplitude information from the offset output signal. Feedback phase

15 detector 114 may be a composite phase detector that detects the phase difference between two periodic signals. Origin-offset signal generator 124 generates the origin-offset signal, which may be an RF signal. The origin-offset signal may be a sine wave at the output frequency and may contain, for example harmonics. The origin-offset signal may also be a square wave or other signal with proper

20 filtering. Carrier leakage compensation element 124 may compensate the origin-offset signal for any origin mismatch.

In one embodiment, signal synthesizer 118 may synthesize an output signal at the same frequency as the input signal. For example, both the input and the output signals may be IF frequencies. In another embodiment, signal

25 synthesizer 118 may synthesize an output signal having a different frequency than the input signal. For example, the input signal may be an IF signal and signal synthesizer 118 may synthesize an RF or other higher frequency signal. In this embodiment, element 126 may also include functionality to down-convert the origin-offset signal to the frequency of the input signal. Alternatively, carrier

30 leakage compensation element 126 may be implemented within a digital signal processor which adds the origin-offset signal directly to the input signal. A live adaptation process may be used to correlate between the output and input origin offset. Signal synthesizer 118 may also synthesize an output signal having a

different amplitude than the input signal and an attenuator may be included to help equalize the average amplitude of the feedback signal.

Transmitter 100 may also include signal processor 130 which, among other things, may control the amplitude and phase components of the origin-offset signal generated by origin offset generator 124. Signal processor 130 may also control an amount of compensation of the origin-offset signal by carrier leakage compensation element 126. Signal processor 130 may be implemented as part of a digital signal processor (DSP) and may be configured with software and firmware. Although signal processor 130 is illustrated in FIG. 1 as a separate functional element, other functional elements of transmitter 100 may also be implemented as part of a DSP. For example, a portion of carrier leakage compensation element 126 and portions of origin-offset signal generator 124 may also be implemented as part of the signal processor 130. In one embodiment, detectors 106, 108, 114 and 116, signal synthesizer 118, and elements 110 and 112 may also be implemented within one or more DSPs.

Transmitter 100 helps reduce and even may eliminate the difficulties associated with zero-crossings of a conventional polar-loop transmitter by shifting the origin of the complex signal away from the true origin. Because the origin shifting signal is provided at both the input to the control loop and in the feedback branch, the output is not origin-shifted. Mismatch in the origin shift may lead to carrier leakage at the output signal, however compensation may also be provided by carrier leakage compensation element 126.

Signal processor 130 among other things, may control the amplitude and phase components of the origin-offset signal generated by origin offset generator 124. The control of the origin-offset signal may be based on the output signal from coupling element 128 and may be set to shift the signal trajectory away from zero on the phasor plane. For example, it may be set with an angle of 45 degrees or greater to avoid a zero-crossing. The proportion of the origin-offset signal to the output signal may be a predetermined number, and may be adapted to output levels proportionally. The transmitted signal may also be down-converted and the carrier leakage may be detected as a DC component.

Signal processor 130 may also control an amount of compensation of the origin-offset signal by carrier leakage compensation element 126. For example, signal processor 130 may adjust the amplitude and phase of the compensation

signal provided by element 126 based on the transmitted signal. In one embodiment, a ratio of RMS level to average levels of the output signal amplitude may be used to determine an appropriate carrier leakage compensation level to help compensate for origin mismatch.

5   The relative amplitude and phase may be substantially matched on the forward and feedback paths. In one embodiment, the relative level of the amplitude and amount of phase may be adapted by signal processor 130 based on feedback, for example, when higher accuracy is desired.

Non-linear amplifier 120 may be any non-linear amplifier including RF or
10   microwave power amplifiers or other non-linear amplifiers specific to the application of transmitter 100. Phase detectors 106 and 114 may, for example, comprise phase locked loops, and amplitude detectors 108 and 116 may be envelope detectors. Signal synthesizer 118 may include components such as a voltage controller oscillator (VCO) and amplitude modulator to synthesize an
15   output signal from phase and amplitude reference signals. Combining elements 104 and 122 may be signal combiners. In one embodiment, combining elements 104 and 122 may be implemented as part of a DSP in which the combining may be accomplished by current summation.

Transmitter 100 may be used for modulating and amplifying an
20   information signal for further transmission through a radio channel. In one or more embodiments, transmitter 100 may be implemented as part of a mobile or wireless communication device, such as wireless telephone. In another embodiment, transmitter 100 may be implemented as part of communication base stations for providing wireless communications to wireless communication
25   devices. In other embodiments, transmitter 100 may serve as a transmitter in a hybrid-fiber-coax (HFC) communication system, a cable television system, or a satellite communication system. In one embodiment, transmitter 100 may implement one or more of many communication techniques including, for example, time-division multiple-access (TDMA) communications, frequency-
30   division multiple-access communications (FDMA), code-division multiple-access communications (CDMA), wideband code-division multiple-access communications (WCDMA), and combinations thereof.

In one embodiment, the present invention may provide a digital signal processor (DSP). The DSP may include a phase difference block to generate a

phase reference signal from phase information extracted from an offset input signal and an offset output signal. The DSP may also include an amplitude difference block to generate an amplitude reference signal from amplitude information extracted from the offset input signal and the offset output signal. The

5   DSP may also include a signal synthesizer block to synthesize an output signal from the amplitude reference signal and the phase reference signal. The DSP may also include an input-combining block to add an input signal with an origin-offset signal to produce the offset input signal. The DSP may also include a carrier leakage compensation block to adjust at least one of an amplitude and phase of

10   the origin-offset signal based on a carrier leakage level of the output signal to provide a compensated origin-offset signal to the input-combining block.

FIG. 2 is a flow chart of an output signal generation procedure in accordance with an embodiment of the present invention. Although the individual operations of procedure 200 are illustrated and described as separate operations, it

15   should be noted that one or more of the individual operations may be performed concurrently. Further, nothing necessarily requires that the operations be performed in the order illustrated. Transmitter 100 (FIG. 1) is an example of a transmitter suitable for use in performing procedure 200, however other transmitter configurations may also be suitable.

20   Operation 202 generates an origin-offset signal and operation 204 combines the origin-offset signal with a sampled output signal to produce an offset output signal. Operation 206 compensates the origin-offset signal for any mismatch in the origin shift. In one embodiment, operation 206 may down-convert the origin-offset signal from an RF to an IF frequency. Operation 208

25   combines the origin-offset signal, which may have been compensated in operation 206, with an input signal to produce an offset input signal. Operation 210 extracts phase and amplitude information from the offset input signal. Operation 212 extracts phase and amplitude information from the offset output signal. Operation 214 generates phase and amplitude reference signals from, respectively, the phase

30   and amplitude information extracted from the offset input signal and offset output signal. Operation 216 synthesizes an output signal from the phase and amplitude reference signals, and operation 218 amplifies the output signal with a non-linear amplifier. The non-linearly amplified signal produced in operation 218 may be the

signal that is sampled or coupled as part of operation 204 and combined with the origin-offset signal.

Thus, an improved transmitter and method of generating an output signal have been described. In one embodiment, the transmitter and method may help

5 improve efficiency of a transmitter's non-linear amplifier, and may help utilize the higher efficiency regions of the non-linear amplifier. In another embodiment, the transmitter and method may help reduce the broadening of the frequency spectrum. In another embodiment, the transmitter and method may generate an output signal with improved linearity.

10 The foregoing description of the specific embodiments reveals the general nature of the invention sufficiently that others can, by applying current knowledge, readily modify and/or adapt it for various applications without departing from the generic concept, and therefore such adaptations and modifications are intended to be comprehended within the meaning and range of

15 equivalents of the disclosed embodiments.

It is to be understood that the phraseology or terminology employed herein is for the purpose of description and not of limitation. Accordingly, the invention is intended to embrace all such alternatives, modifications, equivalents and variations as fall within the spirit and broad scope of the appended claims.

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